

# YN-yn Xfmr in Zero Sequence

- use 3 single phase ideal Xfmr
- reference pri and sec windings to neutral
- model pri and sec impedances in series with windings\*
- add a zero sequence source to primary windings
- short the secondary windings to neutral
- all quantities are per-unit
- when using per-unit system for analysis:

$$V_p = V_s = V_{source} - I_p^0 Z_p^0 = 1 - I_p^0 Z_p^0$$

because  $P_{in} = P_{out}$   
 $I_p^0 = I_s^0$

we are wanting the phase impedance  
 "seen" by the source voltage:  $Z_{in}^0$

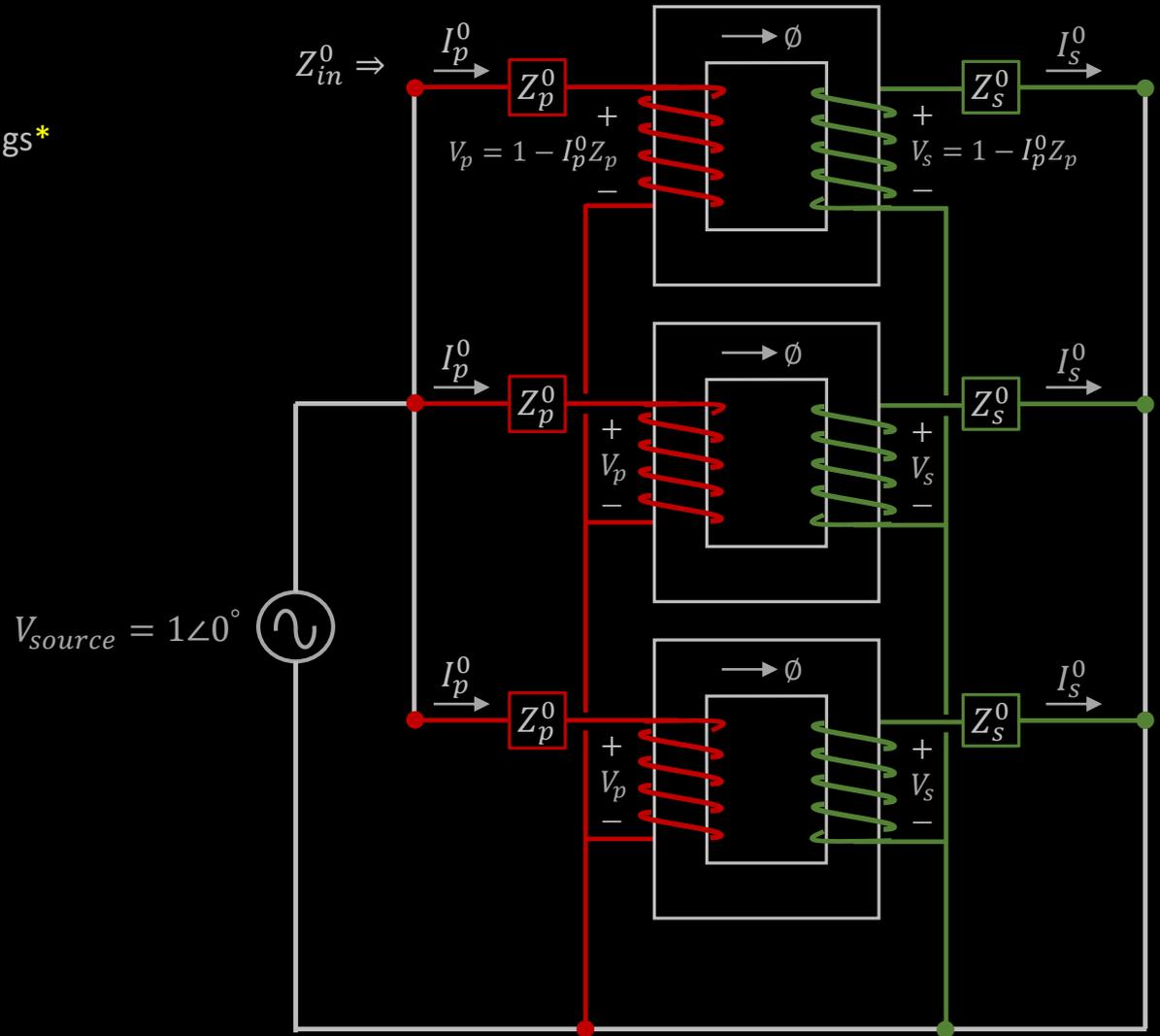
on the primary side:

$$Z_{in}^0 = \frac{V_s}{I_p^0} = \frac{1}{I_p^0}$$

$$I_p^0 = \frac{1}{Z_{in}^0}$$

on the secondary side:

$$I_s^0 = \frac{V_s}{Z_s^0} = \frac{1 - I_p^0 Z_p^0}{Z_s^0}$$



\* it should be noted that  $Z_p$  and  $Z_s$  are not reported separately in a manufacturer test report. instead  $Z_{ps}$  is reported and is equal to  $Z_p + Z_s$

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because  $P_{in} = P_{out}$

$$I_p^0 = I_s^0$$

$$I_p^0 = \frac{1 - I_p^0 Z_p^0}{Z_s^0}$$

$$I_p^0 = \frac{1}{Z_s^0} - \frac{I_p^0 Z_p^0}{Z_s^0}$$

$$I_p^0 + \frac{I_p^0 Z_p^0}{Z_s^0} = \frac{1}{Z_s^0}$$

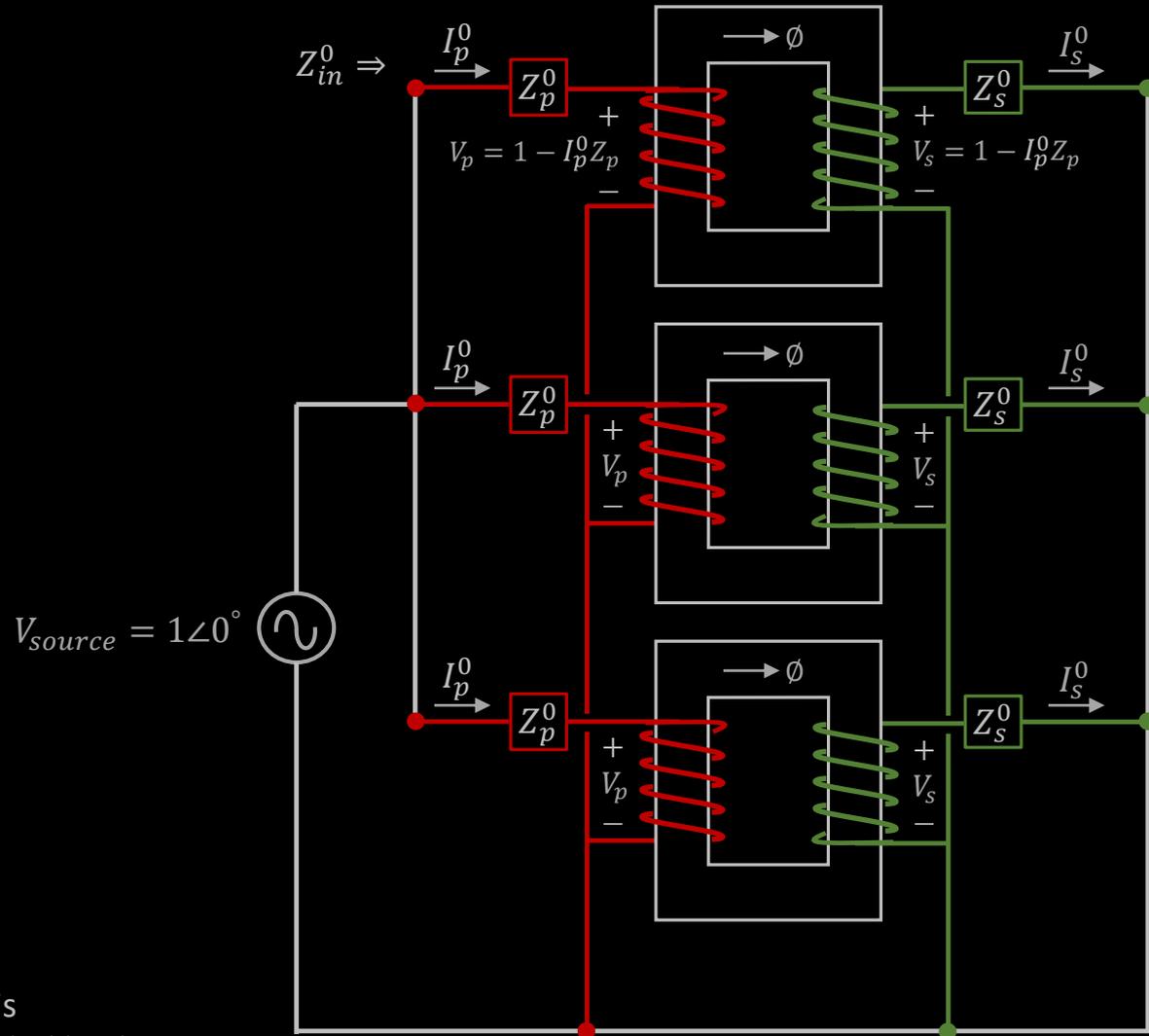
$$I_p^0 \left[ 1 + \frac{Z_p^0}{Z_s^0} \right] = \frac{1}{Z_s^0}$$

$$I_p^0 = \frac{1}{Z_s^0 \left( 1 + \frac{Z_p^0}{Z_s^0} \right)}$$

$$I_p^0 = \frac{1}{Z_s^0 + Z_p^0}$$

$$Z_{in}^0 = \frac{1}{I_p^0} = Z_s^0 + Z_p^0$$

$$Z_{in}^0 = Z_s^0 + Z_p^0$$



$$V_{source} = 1 \angle 0^\circ$$

$$Z_{in}^0 = Z_p^0 + Z_s^0 = Z_{ps}^0$$

nothing remarkable here...

you simply add up the primary and secondary pu impedances

So when performing a per-phase analysis in zero sequence, the YY transformer looks like this:





ΕΦΕΕ

*Dedicated to Power Engineering*

Questions or Comments ...

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