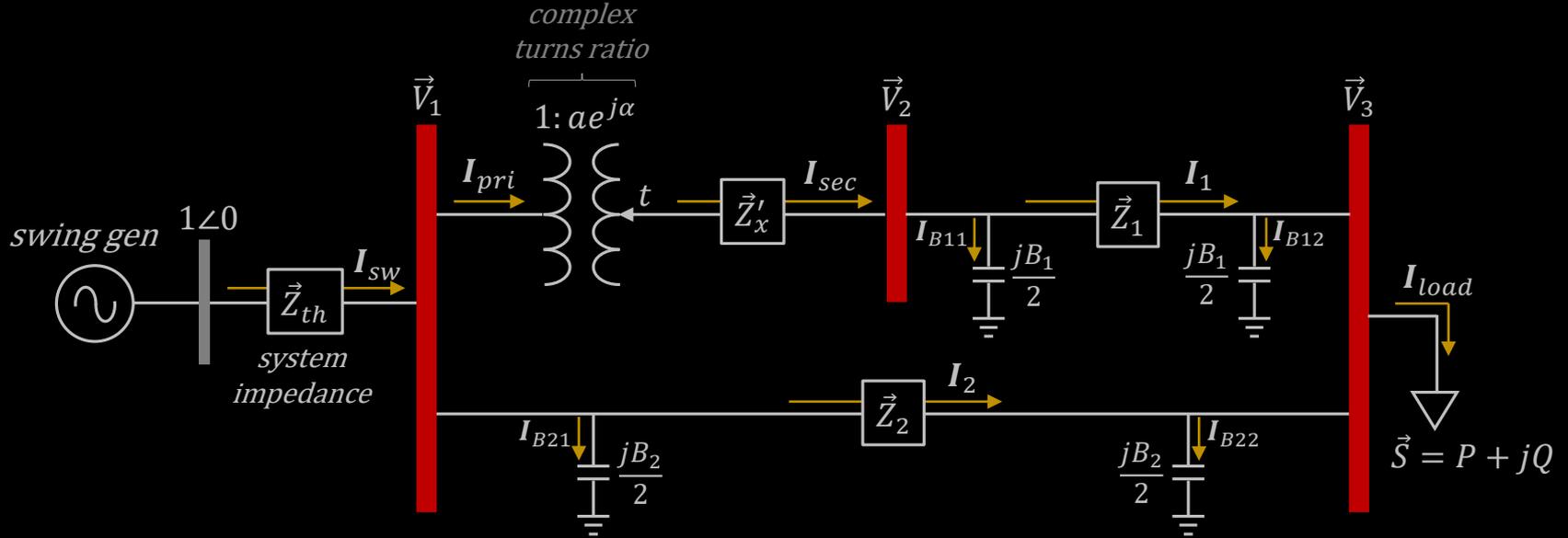


Phase Shifting Xfmr Power Flow

all values per-unit



$\alpha = \text{pst phase shift angle}$

$$a = \sqrt{1 + [\tan \alpha]^2} = \frac{|V_{\text{sec}}|}{|V_{\text{pri}}|}$$

if symmetrical pst...

$$a = 1$$

$t = 1 + \tan \alpha = \text{tap setting}$

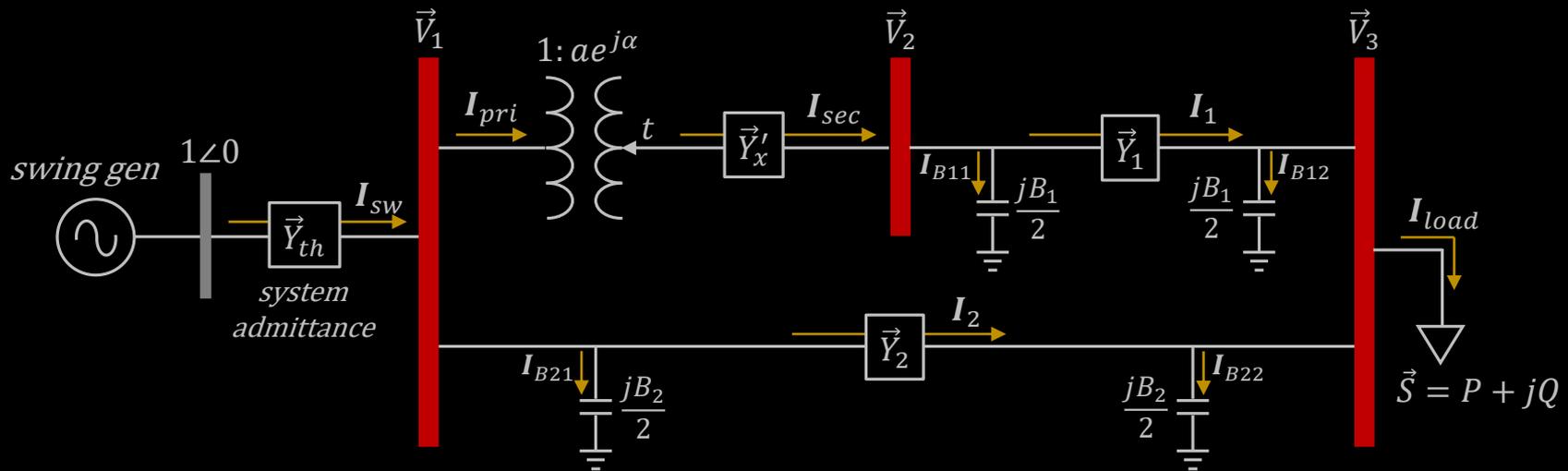
$$\vec{Z}'_x = t^2 \vec{Z}_x$$

KCL ...

Bus1	Bus2	Bus3
$I_{\text{sw}} = I_{\text{pri}} + I_{B21} + I_2$	$I_{\text{sec}} = I_{B11} + I_1$	$I_{\text{load}} = I_1 - I_{B12} + I_2 - I_{B22} = \frac{\vec{S}^*}{\vec{V}_3^*}$

Phase Shifting Xfmr Power Flow (cont.)

convert impedances to admittances



first look at pst current

$$\vec{V}_1 \mathbf{I}_{pri}^* = ae^{j\alpha} \vec{V}_1 \mathbf{I}_{sec}^*$$

$$\mathbf{I}_{pri} = ae^{-j\alpha} \mathbf{I}_{sec}$$

$$\mathbf{I}_{sec} = [ae^{j\alpha} \vec{V}_1 - \vec{V}_2] \vec{Y}'_x$$

$$\mathbf{I}_{pri} = ae^{-j\alpha} [ae^{j\alpha} \vec{V}_1 - \vec{V}_2] \vec{Y}'_x$$

$$\mathbf{I}_{pri} = [a^2 \vec{V}_1 - ae^{-j\alpha} \vec{V}_2] \vec{Y}'_x$$

initially guess that...

$$\vec{V}_1 = \vec{V}_2 = \vec{V}_3 = 1 \angle 0$$

then use...

\vec{V}_2 and \vec{V}_3

to get new \vec{V}_1 \longrightarrow

then iterate with Gauss-Seidel method

KCL @ Bus1

$$\mathbf{I}_{sw} = \mathbf{I}_{pri} + \mathbf{I}_{B21} + \mathbf{I}_2$$

$$[1 - \vec{V}_1] \vec{Y}_{th} = [a^2 \vec{V}_1 - ae^{-j\alpha} \vec{V}_2] \vec{Y}'_x + \frac{jB_2}{2} \vec{V}_1 + [\vec{V}_1 - \vec{V}_3] \vec{Y}_2$$

$$\vec{Y}_{th} - \vec{V}_1 \vec{Y}_{th} = a^2 \vec{V}_1 \vec{Y}'_x - ae^{-j\alpha} \vec{V}_2 \vec{Y}'_x + \frac{jB_2}{2} \vec{V}_1 + \vec{V}_1 \vec{Y}_2 - \vec{V}_3 \vec{Y}_2$$

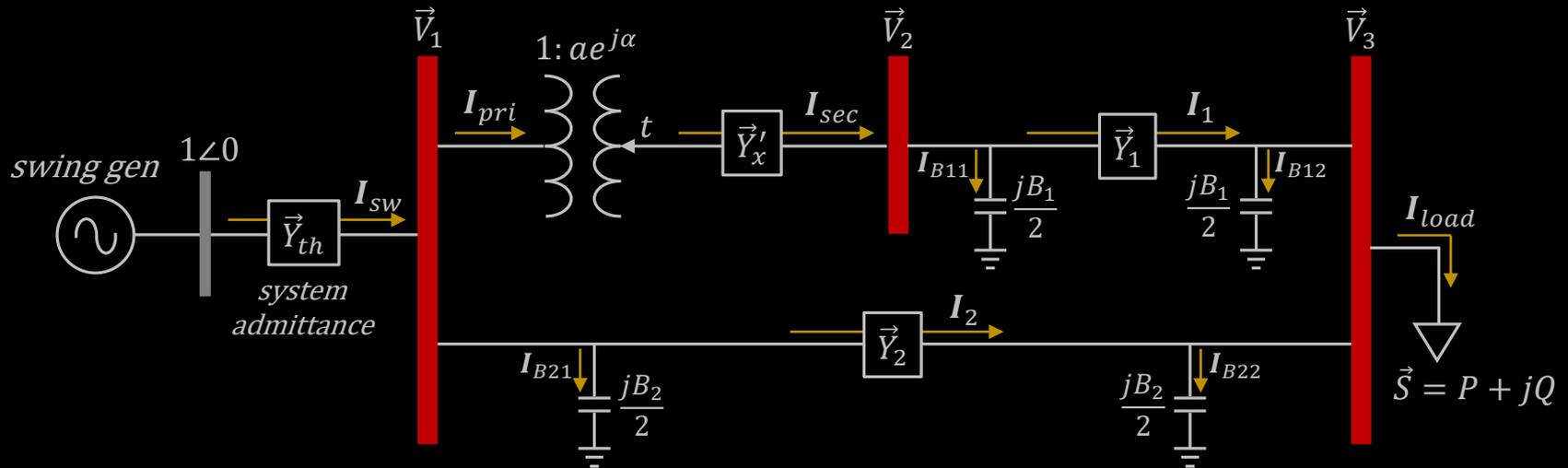
$$-\vec{V}_1 \vec{Y}_{th} - \vec{V}_1 \vec{Y}_2 - a^2 \vec{V}_1 \vec{Y}'_x - \frac{jB_2}{2} \vec{V}_1 = -ae^{-j\alpha} \vec{V}_2 \vec{Y}'_x - \vec{V}_3 \vec{Y}_2 - \vec{Y}_{th}$$

$$\vec{V}_1 \vec{Y}_{th} + \vec{V}_1 \vec{Y}_2 + a^2 \vec{V}_1 \vec{Y}'_x + \frac{jB_2}{2} \vec{V}_1 = ae^{-j\alpha} \vec{V}_2 \vec{Y}'_x + \vec{V}_3 \vec{Y}_2 + \vec{Y}_{th}$$

$$\vec{V}_1 \left[\vec{Y}_{th} + \vec{Y}_2 + a^2 \vec{Y}'_x + \frac{jB_2}{2} \right] = ae^{-j\alpha} \vec{V}_2 \vec{Y}'_x + \vec{V}_3 \vec{Y}_2 + \vec{Y}_{th}$$

$$\vec{V}_1 = \frac{ae^{-j\alpha} \vec{V}_2 \vec{Y}'_x + \vec{V}_3 \vec{Y}_2 + \vec{Y}_{th}}{\vec{Y}_{th} + \vec{Y}_2 + a^2 \vec{Y}'_x + \frac{jB_2}{2}}$$

Phase Shifting Xfmr Power Flow (cont.)



KCL @ Bus2

$$I_{sec} = I_{B11} + I_1$$

$$[ae^{j\alpha}\vec{V}_1 - \vec{V}_2]\vec{Y}'_x = \frac{jB_1}{2}\vec{V}_2 + [\vec{V}_2 - \vec{V}_3]\vec{Y}_1$$

$$ae^{j\alpha}\vec{V}_1\vec{Y}'_x - \vec{V}_2\vec{Y}'_x = \frac{jB_1}{2}\vec{V}_2 + \vec{V}_2\vec{Y}_1 - \vec{V}_3\vec{Y}_1$$

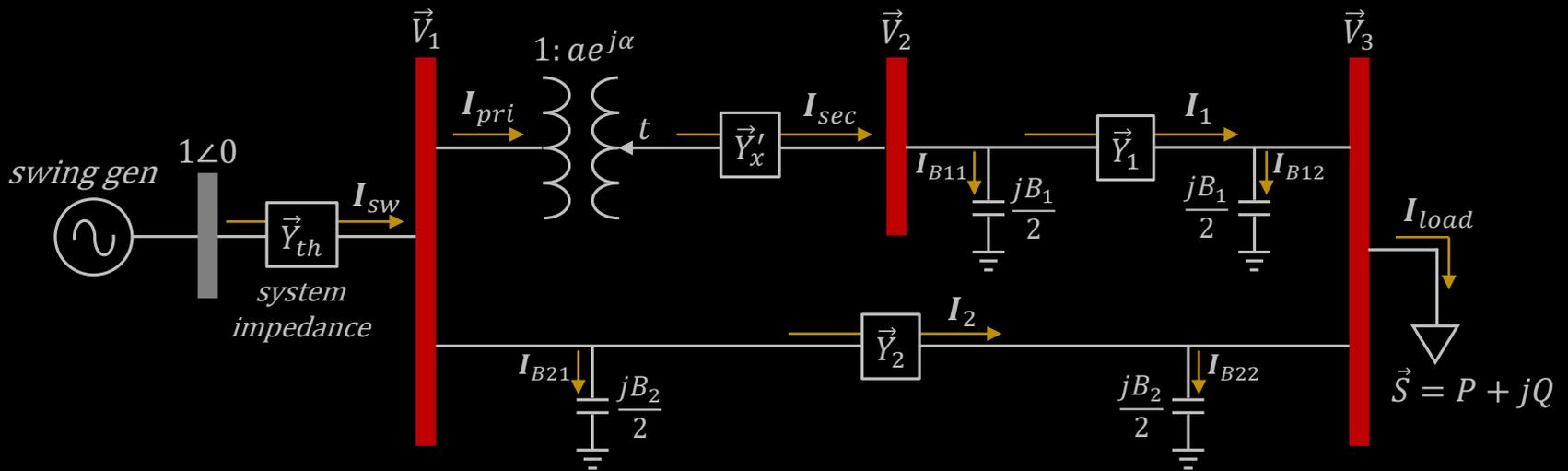
$$-\vec{V}_2\vec{Y}'_x - \vec{V}_2\vec{Y}_1 - \frac{jB_1}{2}\vec{V}_2 = -\vec{V}_3\vec{Y}_1 - ae^{j\alpha}\vec{V}_1\vec{Y}'_x$$

$$\vec{V}_2 \left[\vec{Y}'_x + \vec{Y}_1 + \frac{jB_1}{2} \right] = \vec{V}_3\vec{Y}_1 + ae^{j\alpha}\vec{V}_1\vec{Y}'_x$$

use new \vec{V}_1 and last known \vec{V}_3
to get new \vec{V}_2

$$\vec{V}_2 = \frac{\vec{V}_3\vec{Y}_1 + ae^{j\alpha}\vec{V}_1\vec{Y}'_x}{\vec{Y}'_x + \vec{Y}_1 + \frac{jB_1}{2}}$$

Phase Shifting Xfmr Power Flow (cont.)



use new \vec{V}_1 and \vec{V}_2 and last known \vec{V}_3
to get new \vec{V}_3



$$\vec{V}_3 = \left[\frac{-\vec{S}^*}{\vec{V}_3^*} + \vec{V}_1 \vec{Y}_2 + \vec{V}_2 \vec{Y}_1 \right] \left[\frac{1}{\vec{Y}_1 + \vec{Y}_2 + \frac{jB_1}{2} + \frac{jB_2}{2}} \right]$$

KCL @ Bus3

$$I_1 - I_{B12} + I_2 - I_{B22} = \frac{\vec{S}^*}{\vec{V}_3^*}$$

$$[\vec{V}_2 - \vec{V}_3] \vec{Y}_1 - \frac{jB_1}{2} \vec{V}_3 + [\vec{V}_1 - \vec{V}_3] \vec{Y}_2 - \frac{jB_2}{2} \vec{V}_3 = \frac{\vec{S}^*}{\vec{V}_3^*}$$

$$\vec{V}_2 \vec{Y}_1 - \vec{V}_3 \vec{Y}_1 - \frac{jB_1}{2} \vec{V}_3 + \vec{V}_1 \vec{Y}_2 - \vec{V}_3 \vec{Y}_2 - \frac{jB_2}{2} \vec{V}_3 = \frac{\vec{S}^*}{\vec{V}_3^*}$$

$$-\vec{V}_3 \vec{Y}_1 - \vec{V}_3 \vec{Y}_2 - \frac{jB_1}{2} \vec{V}_3 - \frac{jB_2}{2} \vec{V}_3 = \frac{\vec{S}^*}{\vec{V}_3^*} - \vec{V}_1 \vec{Y}_2 - \vec{V}_2 \vec{Y}_1$$

$$\vec{V}_3 \vec{Y}_1 + \vec{V}_3 \vec{Y}_2 + \frac{jB_1}{2} \vec{V}_3 + \frac{jB_2}{2} \vec{V}_3 = \frac{-\vec{S}^*}{\vec{V}_3^*} + \vec{V}_1 \vec{Y}_2 + \vec{V}_2 \vec{Y}_1$$

$$\vec{V}_3 \left[\vec{Y}_1 + \vec{Y}_2 + \frac{jB_1}{2} + \frac{jB_2}{2} \right] = \frac{-\vec{S}^*}{\vec{V}_3^*} + \vec{V}_1 \vec{Y}_2 + \vec{V}_2 \vec{Y}_1$$

leave conjugate here

pseudo code for pst power flow analysis

```
given: alpha_rad, yth, yx, y1, y2, b1, b2, s
v1 = v2 = v3 = 1<0
tol = 1e-6
iteration = 0
max_iterations = 99
converged = False
while not converged and iteration < max_iterations:
    converged = True
    iteration += 1
    new_v1 = f(v2,v3)
    new_v2 = f(new_v1,v3)
    new_v3 = f(new_v1, new_v2)
    delta_v1 = abs(new_v1 - v1)
    delta_v2 = abs(new_v2 - v2)
    delta_v3 = abs(new_v3 - v3)
    v1 = new_v1
    v2 = new_v2
    v3 = new_v3
    if delta_v1 > tol:
        converged = False
    elif delta_v2 > tol:
        converged = False
    elif delta_v3 > tol:
        converged = False
# yth, yx, y1, y2, b1, b2, s (complex)
# first guess (complex)
# assign convergence tolerance
# initialize number of iterations
# assign max iterations
# set converged flag = False
# loop while not converged
# assume converged
# increment iteration
# get new v1
# get new v2
# get new v3
# get magnitude of v1 change
# get magnitude of v2 change
# get magnitude of v3 change
# assign new_v1 to v1
# assign new_v2 to v2
# assign new_v3 to v3
# if v1 change > tolerance...
# set convergence flag = False
# if v2 change > tolerance ...
# set convergence flag = False
# if v3 change > tolerance ...
# set convergence flag = False
```

```
if converged:
    all bus voltage magnitudes and angles are known...
    everything else can be calculated
```



ΞΦΕΕ

Dedicated to Power Engineering

Questions or Comments ...

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