

# Compensated Bus Voltage Change Derivation

$$\overrightarrow{MVA}_{SC} = V_S \vec{I}_{SC}^* \quad \vec{I}_{SC} = \frac{V_S}{Z_S} \quad \overrightarrow{MVA}_{SC} = \frac{|V_S|^2}{\vec{Z}_S^*} \quad \vec{Z}_S^* = \frac{|V_S|^2}{\overrightarrow{MVA}_{SC}}$$

$$\vec{S} = \vec{V}_B \vec{I}^* \quad \vec{I}^* = \frac{\vec{S}}{\vec{V}_B}$$

$$I = \frac{V_S - \vec{V}_B}{\vec{Z}_S} \quad \vec{I}^* = \frac{V_S - \vec{V}_B^*}{\vec{Z}_S^*}$$

$$\frac{\vec{S}}{\vec{V}_B} = \frac{V_S - \vec{V}_B^*}{\vec{Z}_S^*}$$

$$\vec{S} \vec{Z}_S^* = V_S \vec{V}_B - \vec{V}_B^* \vec{V}_B$$

$$|V_B|^2 - V_S \vec{V}_B + \vec{S} \vec{Z}_S^* = 0$$

$$|V_B|^2 - V_S \vec{V}_B + \frac{\vec{S} |V_S|^2}{\overrightarrow{MVA}_{SC}} = 0$$

Assume:  $|V_S|^2 \approx |V_B|^2$

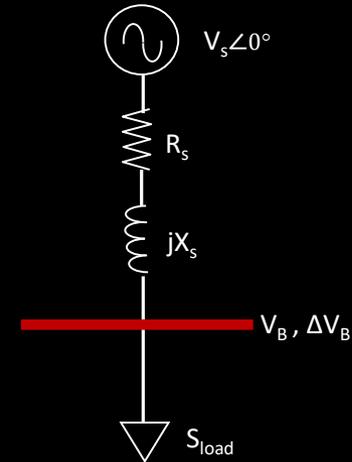
$$|V_B|^2 - V_S \vec{V}_B + \frac{\vec{S} |V_B|^2}{\overrightarrow{MVA}_{SC}} = 0 \quad \text{Let } \vec{A} = \frac{\vec{S}}{\overrightarrow{MVA}_{SC}}$$

$$|V_B|^2 + \vec{A} |V_B|^2 - V_S |V_B| e^{j\theta_B} = 0$$

$$(\vec{A} + 1) |V_B|^2 - V_S |V_B| e^{j\theta_B} = 0$$

Assume:  $\theta_B \approx \theta_S = 0$

$$(\vec{A} + 1) |V_B|^2 - V_S |V_B| = 0 \quad \leftarrow$$



use quadratic form:

$$V_B = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$V_B = \frac{V_S \pm \sqrt{V_S^2 - 4(\vec{A} + 1)0}}{2(\vec{A} + 1)} = \frac{V_S \pm V_S}{2(\vec{A} + 1)} = \frac{2V_S}{2(\vec{A} + 1)} = \frac{V_S}{(\vec{A} + 1)}$$

$$\vec{V}_B = \frac{V_S}{\vec{A} + 1}$$

$$\frac{\Delta \vec{V}_B}{\vec{V}_{B0}} = \frac{\vec{V}_{Bf} - \vec{V}_{B0}}{\vec{V}_{B0}}$$

$$\vec{V}_{B0} = \frac{V_S}{\vec{A}_0 + 1}$$

$$\vec{V}_{Bf} = \frac{V_S}{\vec{A}_f + 1}$$

$$\frac{\Delta \vec{V}_B}{\vec{V}_{B0}} = \frac{\frac{V_S}{\vec{A}_f + 1} - \frac{V_S}{\vec{A}_0 + 1}}{\frac{V_S}{\vec{A}_0 + 1}} = \frac{\vec{A}_0 + 1}{\vec{A}_f + 1} - 1 = \frac{\vec{A}_0 - \vec{A}_f}{\vec{A}_f + 1}$$

$$\vec{A}_0 = \frac{\vec{S}_0}{\overline{MVAS_C}} \quad \vec{A}_f = \frac{\vec{S}_f}{\overline{MVAS_C}}$$

$$\frac{\Delta \vec{V}_B}{\vec{V}_{B0}} = \frac{\frac{\vec{S}_0}{\overline{MVAS_C}} - \frac{\vec{S}_f}{\overline{MVAS_C}}}{\frac{\vec{S}_f}{\overline{MVAS_C}} + 1} = \frac{\vec{S}_0 - \vec{S}_f}{\vec{S}_f + \overline{MVAS_C}}$$

$$\vec{S}_0 = P + jQ$$

$$\vec{S}_f = P + jQ + j\Delta Q$$

$$\frac{\Delta \vec{V}_B}{\vec{V}_{B0}} = \frac{P + jQ - (P + jQ + j\Delta Q)}{P + jQ + j\Delta Q + \overline{MVAS_C}} = \frac{-j\Delta Q}{P + jQ + j\Delta Q + \overline{MVAS_C}}$$

Q is positive if load is inductive  
Q is negative if load is capacitive

$\Delta Q$  is positive if adding inductor  
 $\Delta Q$  is negative if adding capacitor

$$\frac{\overrightarrow{\Delta V}_B}{\overrightarrow{V}_{B0}} = \frac{-j\Delta Q}{P + jQ + j\Delta Q + \overrightarrow{MVA}_{SC}}$$

if  $X_s \gg R_s$ :

$$\overrightarrow{MVA}_{SC} = j|MVA_{SC}|$$

$$\frac{\overrightarrow{\Delta V}_B}{\overrightarrow{V}_{B0}} = \frac{-j\Delta Q}{P + jQ + j\Delta Q + j|MVA_{SC}|} = \frac{-j\Delta Q}{P + j(|MVA_{SC}| + Q + \Delta Q)}$$

$$\frac{|\overrightarrow{\Delta V}_B|}{|\overrightarrow{V}_{B0}|} = \frac{-\Delta Q}{\sqrt{P^2 + (MVA_{SC} + Q + \Delta Q)^2}}$$

if  $MVA_{SC} \gg P_{load}, Q_{load}$

$$\frac{|\overrightarrow{\Delta V}_B|}{|\overrightarrow{V}_{B0}|} \approx \frac{-\Delta Q}{MVA_{SC}}$$

Q is positive if load is inductive  
Q is negative if load is capacitive

$\Delta Q$  is positive if adding inductor  
 $\Delta Q$  is negative if adding capacitor

## Summary

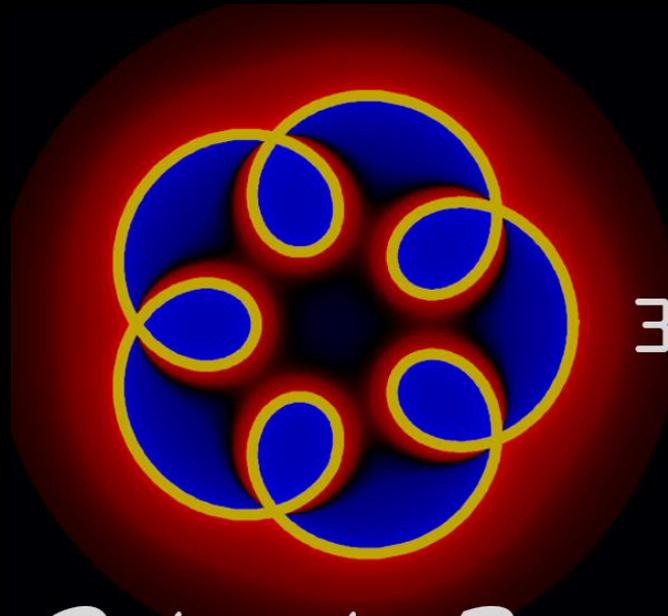
This derivation reveals that the amount of voltage change due to switching reactive compensation is dependent on system strength. Keep in mind that during outage conditions, the system strength could be greatly reduced, resulting in much larger change in voltage.

$$\left| \frac{\overrightarrow{\Delta V}_B}{\overrightarrow{V}_{B0}} \right| = \frac{-\Delta Q}{\sqrt{P^2 + (MVA_{SC} + Q + \Delta Q)^2}}$$

$$\left| \frac{\overrightarrow{\Delta V}_B}{\overrightarrow{V}_{B0}} \right| \approx \frac{-\Delta Q}{MVA_{SC}}$$

This one is actually a very good approximation. System voltage magnitude and thevenin impedance would be needed for an exact solution of a very complex equation.

This one is a very common approximation. Assumes that the load MVA is much less than the short circuit MVA, which is usually true.



ΞΦΕΕ

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Questions or Comments ...

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